

Backstepping Techniques for PDE Control: From Fundamentals to Open Problems

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Largely based on the 2026 Automatica paper
Backstepping for partial differential equations: A survey
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Why control systems modeled by PDEs?

PDEs model systems that vary in *space and time*

- traffic flow, heat & chemical reactors, flexible structures
- batteries, drilling, plasmas, fluid flows

We often want to **stabilize**, **estimate**, or **improve performance**

Yet ready-to-use, systematic design tools have historically been scarce

Backstepping offers a **constructive**, often **explicit** answer for boundary control

What this talk is (and is not)

Goal: build intuition for the backstepping method, survey where the field is going, and open today's program

Three parts:

- **Fundamentals:** the method on one paradigmatic example
- **Adaptations & applications:** what the basic recipe needs in practice
- **Open problems:** where a starting researcher can contribute

Boundary control of 1-D linear PDEs is the backbone; pointers to the rest.

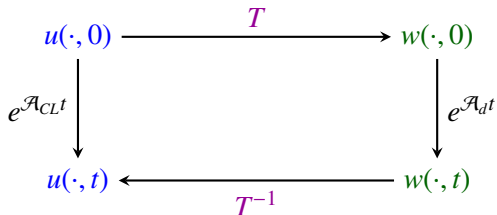
This is **not** a complete overview (time constraints) nor can we cite hundreds of papers (go read the survey!)

Part I: Fundamentals

The method in one picture, on one example

Backstepping in one picture

Main idea: do not tackle the original (unstable/difficult-to-solve) PDE directly. *Change coordinates* so that it becomes a system you already know is stable



plant $\xrightarrow{T}$ stable target system

If T is **bounded** and **boundedly invertible**, the two share stability properties (Smyshlyaev and Krstic, 2004)

A paradigmatic plant: reaction-diffusion

Consider a reaction-diffusion PDE on $x \in [0, 1]$:

$$u_t = \epsilon u_{xx} + \lambda(x)u, \quad u(t, 0) = 0, \quad u(t, 1) = U(t)$$

- $\epsilon > 0$: diffusion $\lambda(x)$: reaction (may be *destabilizing*)
- $U(t)$: boundary actuation (the only place where we can act!)

Open loop ($U = 0$): a Lyapunov estimate with $L(t) = \frac{1}{2}\|u\|_{L^2}^2$ gives

$$\|u(t)\|_{L^2}^2 \leq e^{-(\frac{\epsilon}{2} - 2\bar{\lambda})t} \|u(0)\|_{L^2}^2$$

exponentially stable if $\bar{\lambda} := \max_x \lambda < \epsilon/4$ (not sharp); a large reaction can destabilize, and then we must act

The three interlinked ingredients

A backstepping design rests on **three** key elements (Smyshlyaev and Krstic, 2004):

- 1 a **target system** with the properties we want (e.g., stability)
- 2 a **transformation** mapping **plant** $\rightarrow$ **target**, bounded & invertible
- 3 **kernel equations**: the conditions the transform must satisfy

They are **coupled**: a good target $\Rightarrow$ solvable kernels + invertible transform. A bad target $\Rightarrow$ no solution or not invertible.

Step 1: choosing the target system

For our plant, a natural target neutralizes the reaction term and adds a degree of freedom:

$$w_t = \epsilon w_{xx} - c w, \quad w(t, 0) = 0, \quad w(t, 1) = 0$$

exponentially stable for any $c \geq 0$ (decay rate tunable via c)

Design principles

- *keep the nature of the system (still reaction-diffusion, same ϵ)*
- *keep the boundary conditions (Dirichlet stays Dirichlet)*
- *transform only the destabilizing terms (cancel the reaction or make it stabilizing)*

Similar enough to be reachable, different enough to be stable.

Step 2: the backstepping transformation

ODE backstepping (Krstic, Kanellakopoulos, and Kokotovic, 1995) applied to spatial discretizations of the PDE (Balogh and Krstic; Bošković, Balogh, and Krstić, 2002; 2003) suggests a *spatially causal* (strict-feedback) map:

$$w(t, x) = u(t, x) - \int_0^x k(x, \xi) u(t, \xi) d\xi$$

- a **Volterra** integral (upper limit x): the value at x depends only on $[0, x]$
- Volterra $\Rightarrow$ **always invertible** under mild conditions on k

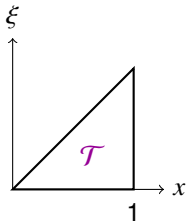
When strict-feedback structure is lost, one needs a **Fredholm** map, and invertibility is no longer free (Part III)

Step 3: the kernel equations

Substitute the transform into the target, integrate by parts: k must solve a hyperbolic PDE on the triangle $\mathcal{T} = \{0 \leq \xi \leq x \leq 1\}$:

$$\epsilon k_{xx} - \epsilon k_{\xi\xi} = (\lambda(\xi) + c) k,$$

$$k(x, 0) = 0, \quad k(x, x) = -\frac{1}{2\epsilon} \int_0^x (\lambda(\xi) + c) d\xi$$



Well-posedness: successive approximations

Change variables, integrate once $\Rightarrow$ an *integral equation* $G = G_0 + \mathcal{K}[G]$

Solve by iterating:

$$k = \lim_{n \rightarrow \infty} G_n, \quad G_n = G_0 + \mathcal{K}[G_{n-1}]$$

Since λ is continuous, the series **converges**: a unique $k \in C^1(\mathcal{T})$

This same recipe (*integral form + successive approximations*) recurs for almost every backstepping design in the talk (Fredholm transforms require a different approach)

The control law (and what it needs)

Evaluate the transform at the actuated boundary $x = 1$, use $w(t, 1) = 0$:

$$U(t) = \int_0^1 k(1, \xi) u(t, \xi) d\xi$$

Observations that matter in practice:

- the *implementation* uses only the **trace** $k(1, \cdot)$; the full kernels k, l still enter the stability and robustness estimates (next slide)
- evaluating a trace demands **regularity**: a bounded k is not enough, in this example, the continuity from $k \in C^1(\mathcal{T})$ makes the gain well-defined
- it needs the **full state** $u(t, \cdot) \Rightarrow$ motivates observers

Why the closed loop is stable

The Volterra transform is invertible: $u = w + \int_0^x l(x, \xi) w d\xi$

Direct + inverse give two-sided norm equivalence:

$$\|w\|_{L^2} \leq (1 + \|k\|_\infty) \|u\|_{L^2}, \quad \|u\|_{L^2} \leq (1 + \|l\|_\infty) \|w\|_{L^2}$$

Theorem

The origin of the closed-loop u -system is exponentially stable in L^2 :

$$\|u(t)\|_{L^2}^2 \leq (1 + \|l\|_\infty)^2 (1 + \|k\|_\infty)^2 e^{-(\frac{\epsilon}{2} + 2c)t} \|u(0)\|_{L^2}^2$$

Decay rate is *chosen*; constant in the estimate grows with the kernel size (a recurring trade-off).

Observers by duality

We rarely measure the whole state. Suppose we only measure $u_x(t, 0)$, at the *unactuated* end (anti-collocated).

Observer = copy of the plant + output-error injection $p_1(x)$:

$$\hat{u}_t = \epsilon \hat{u}_{xx} + \lambda \hat{u} + p_1(x)(u_x(t, 0) - \hat{u}_x(t, 0))$$

The error $\tilde{u} = u - \hat{u}$ is mapped to a stable target by a *dual* backstepping transform; its kernel equations are the *same type* as before (Smyshlyaev and Krstic, 2005)

⇒ the gain p_1 is obtained directly from the observer kernel. Design once, reuse by duality.

Output feedback + other 1-D systems

Combine controller (needs state) with observer (provides estimate):

$$U(t) = \int_0^1 k(1, \xi) \hat{u}(t, \xi) d\xi$$

For linear PDEs the **separation principle** holds: controller + observer is stable.

The *same* three-step recipe extends to:

- first-order hyperbolic (transport) with some non-local terms: target is a pure transport (delay), finite-time stable (Krstic and Smyshlyaev, 2008a)
- wave / beams: introduce damping in the target (Krstic, Siranosian, and Smyshlyaev, 2006)
- complex-valued (Schrödinger): kernels via Bessel/Kelvin functions (Krstic, Guo, and Smyshlyaev, 2011)

Part II: Adaptations & applications

What the basic recipe needs in practice

Interconnected systems: the general picture

Real systems may couple transport, in-domain effects, and lumped (ODE) dynamics:

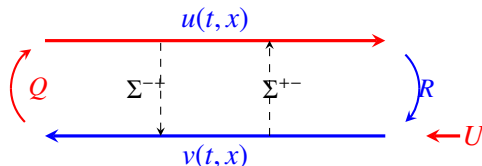
$$\left\{ \begin{array}{l} \dot{X} = A_0 X + B U(t) + E_0 v(t, 0) \quad (\text{actuator ODE}) \\ w_t + \Lambda(x) w_x = \Sigma(x) w, \quad w = (u^\top, v^\top)^\top \\ \dot{Y} = A_1 Y + E_1 u(t, 1) \quad (\text{load ODE}) \\ u(0) = Q v(0) + C_0 X, \quad v(1) = R u(1) + C_1 Y \end{array} \right.$$

u/v : right/left-going states Λ : speeds Σ : in-domain coupling Q, R : boundary reflections

The transform gains block-triangular structure (PDE part + ODE terms), still boundedly invertible

From 2×2 to $n + m$ heterodirectional

n rightward + m leftward transport states, coupled in-domain and at boundaries.



- controllable to zero in minimum time $t_F = \frac{1}{\lambda_1} + \frac{1}{\mu_1}$ (slowest speed each way) (Li and Rao; Coron, Vazquez, Krstic, and Bastin, 2010; 2013)

- $n + m$ case: controllers & observers for the general case (Hu, Di Meglio, Vazquez, and Krstic; Auriol and Di Meglio; Coron, Hu, and Olive, 2016; 2016; 2017)

A crucial caveat: delay-robustness

Method of characteristics rewrites the hyperbolic system as an **Integral Delay Equation** for the transformed state Z at the actuated boundary (Auriol and Di Meglio, 2019):

$$Z(t) = \sum_{i=1}^{n_0} F_i Z(t - \tau_i) + \int_0^{t_F} H(v) Z(t - v) dv + \textcolor{red}{U}$$

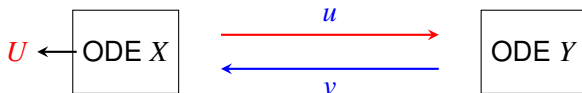
Cancelling *all* reflections gives simple finite-time proofs, but can leave a **zero delay margin** (Auriol, Aarsnes, Martin, and Di Meglio, 2018a)

For robustness: open loop (no Σ , no ODE) already stable; for $n = m = 1$ this is simply $|\rho q| < 1$ (scalar boundary reflections)

$\Rightarrow$ do not over-actuate: keep some reflection, do not demand infinite bandwidth from the actuators

PDE-ODE and ODE-PDE-ODE interconnections

Actuator and/or load dynamics at the boundaries (drilling, delays, flexible structures)



- naive designs cancel everything $\Rightarrow$ robustness lost (Di Meglio, Bribiesca-Argomedeo, Hu, and Krstic; Bou Saba, Bribiesca-Argomedeo, Di Loreto, and Eberard, 2018; 2017)
- robust route: preserve some reflection, rewrite as neutral/IDE, use **filtering** (Auriol, Bribiesca-Argomedeo, Bou Saba, Di Loreto, and Di Meglio; Di Meglio, Lamare, and Aarsnes; Auriol, Bribiesca-Argomedeo, and Di Meglio, 2018b; 2020; 2023a)
- a **strictly proper** controller (low-pass filter) limits bandwidth (Bou Saba, Bribiesca-Argomedeo, Di Loreto, and Eberard, 2019)

More adaptations, at a glance

The same philosophy, retuned for structure:

- **coupled parabolic** $n \times n$: matrix kernels; kernel PDEs mirror the hyperbolic ones (Vazquez and Krstic, 2017)
- **time-varying** coefficients: Gevrey regularity (parabolic) (Vazquez, Trélat, and Coron; Kerschbaum and Deutscher, 2008; 2019) vs. easier hyperbolic (Coron and Nguyen, 2021); gain-scheduling (Auriol and Espitia, 2024)
- **bilateral** control: integrate from the middle of the domain (Vazquez and Krstic, 2016a)
- **beams** (wave & Timoshenko): Riemann transform $\rightarrow$ hyperbolic PDE-ODE (Su, Guo, Wang, and Krstic; Chen, Vazquez, and Krstic, 2017; 2023)
- **higher dimensions**: disks and spheres via symmetry (Vazquez and Krstic; Vazquez and Krstic, 2016b; 2019)
- **adaptive** designs for unknown parameters (Anfinson and Aamo; Smyshlyaev and Krstic, 2019; 2010)

Applications gallery

Backstepping has shown its versatility across many application areas:

- **Traffic:** stop-and-go on freeways (ARZ model), ramp metering (Yu and Krstic; Yu, Auriol, and Krstic, 2019; 2022)
- **Flow control:** Navier-Stokes / MHD channel flows (Vazquez and Krstic; Xu, Schuster, Vazquez, and Krstic, 2007; 2008)
- **Drilling:** axial/torsional vibrations, ODE-PDE-ODE (Aarsnes and van de Wouw; Bresch-Pietri and Krstic, 2019; 2014)
- **Energy:** Li-ion batteries, Stefan (melting) problems (Moura, Chaturvedi, and Krstic; Koga, Diagne, and Krstic, 2013; 2018)
- **Thermo-acoustics:** the Rijke tube (de Andrade, Vazquez, and Pagano, 2018)
- **Multi-agent:** continuum deployment / formation (Frihauf and Krstic, 2010)

Mostly theory/simulation; *experimental* validation so far includes the Rijke tube (de Andrade, Vazquez, and Pagano, 2020), multi-agent robots (Freudenthaler and Meurer, 2020), and a traffic observer on real freeway data (Yu, Gan, Bayen, and Krstic, 2021).

Implementation: solving the kernels

The controller is implementable only after we compute $k(1, \cdot)$:

- **explicit** solutions in special cases (Bessel functions) (Krstic and Smyshlyaev, 2008b)
- **numerics**: finite differences, integral form, or **power series** (Vazquez, Chen, Qiao, and Krstic, 2023a)
- **late lumping**: approximate the controller last; needs stability guarantees
- **neural operators**: learn kernels or gains, with convergence guarantees (Bhan, Shi, and Krstic; Vazquez and Krstic, 2024; 2024)

Part III: Open problems

Where a starting PhD can contribute

Underactuated systems

Almost all designs assume a **fully actuated boundary**.

Underactuated: fewer inputs than boundary states,

$$v(t, 1) = Ru(t, 1) + BU(t) \text{ with } \text{rank}(B) < \dim v$$

- the controllability guarantees behind full actuation (Li and Rao, 2010) no longer apply
- one attempt for a 1 + 2 system with a single input (Auriol, Bribiesca-Argomedo, and Bresch-Pietri, 2020b)
- other results need structural assumptions (cascades) (Auriol; Deutscher, Gehring, and Jung, 2024; 2024)

Largely **open**, and central to networks of PDEs.

In-domain actuation

The Volterra structure made backstepping a **boundary** method by design.

Actuation/sensing *inside* the domain has resisted generic results:

- early parabolic results need special actuator shapes / domain lengths
- hyperbolic results link to **Fredholm** transforms (Redaud and Auriol; Zhang, 2023; 2019)

Progress on Fredholm backstepping (Coron, Hu, and Olive, 2016) may unlock this (some results by the community might be in the works, no spoilers here).

Parametrizable target systems

We usually choose the *simplest* target (cancel everything), but that costs robustness.

What if the target had **tuning parameters**? For instance, for coupled transport equations:

$$\begin{cases} \gamma_t + \Lambda(x)\gamma_x = \bar{\Sigma}(x)\gamma \\ \alpha(0) = Q\beta(0), \quad \beta(1) = \bar{R}\alpha(1) \end{cases}$$

- such targets are always reachable (Redaud, Auriol, and Le Gorrec, 2024);
Port-Hamiltonian ideas guide the choice

- trade off delay-robustness against convergence rate (Auriol, Aarsnes, Di Meglio, and Shor, 2020a); degrees of freedom make the design **modular**

Quantifying the effect of these parameters is open.

Stochastic systems & risk-averse design

Disturbances are usually random, yet most robust designs are *worst-case*.

Early results, in the mean-square sense:

- prediction-based control for ODEs with stochastic input delays (Kong and Bresch-Pietri, 2022)
- stability analysis of 2×2 hyperbolic systems with random parameters (Auriol, Pereira, and Kulcsar, 2023b)

Open: control the **variance**, not just the mean (**risk-averse** backstepping).

Multi-dimensional theory & learning

Despite progress, backstepping remains fundamentally **1-D**.

Multi-D results rely on special geometries (balls, disks, spheres) + **symmetry** (Vazquez and Krstic; Vazquez and Krstic; Vazquez, Zhang, Qi, and Krstic, 2016b; 2019; 2023b)

A general multi-D theory would need:

- target systems in several dimensions
- well-posed multi-D kernel equations + practical solvers

Domain-extension for irregular domains is one promising route (Vazquez, 2025); **neural operators** are a complementary one: learn kernels, keep guarantees.

Conclusions

Backstepping = **target system** + **invertible transform** + **kernel equations**

- constructive, often explicit, with precise closed-loop knowledge
- the same procedure extends from a scalar heat equation to PDE-ODE networks
- key practical lesson: *do not over-actuate* (robustness needs restraint)
- fertile open ground: underactuation, in-domain, stochastic, multi-D, learning

Today's program continues these threads (bridging theory and implementation):

- interconnected PDE-ODE backstepping, systematically: **N. Gehring** (next)
- Port-Hamiltonian target systems: **H. Ramirez, A. Macchelli**
- neural-operator and data-driven PDE control: **Y. Shi, G. A. de Andrade**

Thank you! Questions welcome.

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